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SUPERSONIC AXISYMMETRIC NOZZLE DESIGN BY MASS FLOW TECHNIQUES UTILIZING A DIGITAL COMPUTER

By

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Engineering Support Facility
ARO, Inc.

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ARNOLD ENGINEERING DEVELOPMENT CENTER

AIR FORCE SYSTEMS COMMAND

UNITED STATES AIR FORCE

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a subsidiary of Sverdrup and Parcel, Inc.

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FOREWORD

The authors wish to acknowledge the assistance of James C. Sivells and Clark R. Fitch of the Hypersonic Branch, von Karman Gas Dynamics Facility, ARO, Inc., who initiated the problem, gave valuable suggestions, and supplied the comparison of theoretical and computed results (Fig. 5) in this report.

ABSTRACT

This report presents a method to design the inviscid wall contour of a supersonic, axisymmetric nozzle producing uniform parallel flow at the exit. The calculation methods used are restricted to a perfect gas. The axis velocity distribution must be specified. A complete flow pattern within the nozzle is computed by the method of characteristics beginning at Mach 1.0 on the axis and extending to the region of uniform parallel flow at the exit. The wall points are calculated by means of a mass integration technique. The methods of calculation included have been programmed in Fortran II language, and a complete listing of the program is given in Appendix I.

PUBLICATION REVIEW

This report has been reviewed and publication is approved.

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Mass flow

M

p

q

t

NOMENCLATURE

$\mathbf{m}_{\mathbf{O}}$	Initial mass integration value
P	$\frac{\sin \theta \sin \alpha dy}{\sin (\theta \pm \alpha) y}$
Q	cot α/W
r	Radius
8	Distance along a characteristic
v	Velocity
W	Velocity/limiting velocity (V/V _{max})
X	Physical abscissa
Y	Physical ordinate
α	Mach angle ($\sin \alpha = 1.0/M$ ach number)
γ	Ratio of specific heats
η	Inflection angle
θ	Flow angle (with respect to axis)
ρ	Density
ψ	Prandtl-Meyer angle
SUBSCRIPTS	
1	Refers to right-running characteristic
2	Refers to left-running characteristic
a	Origin of right-running characteristic
b	Origin of left-running characteristic
c	Computed point
B C	End points on line BC
N	Normal Component

Point on line BC

Point on line CD

Total (stagnation condition)

1.0 INTRODUCTION

This report presents a method to design the inviscid wall contour of a supersonic, axisymmetric nozzle producing uniform parallel flow at the exit. The calculation methods used are restricted to a perfect gas. The axis velocity distribution must be specified.

A complete flow pattern within the nozzle is computed by the method of characteristics beginning at Mach 1.0 on the axis and extending to the region of uniform parallel flow at the exit. The wall points are calculated by means of a mass integration technique.

The methods of calculation included in this report have been programmed in Fortran II language, and a complete listing of the program is given in Appendix I. This program has been run on the IBM 7074 computer at the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC), to obtain the results to be presented.

2.0 SCOPE OF CALCULATIONS

For the purpose of calculations the flow in the nozzle is arbitrarily divided into three distinct regions as shown in Fig. 1.

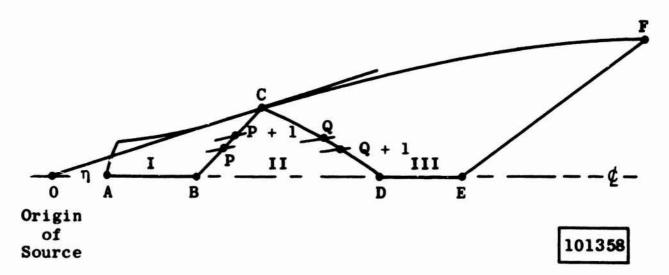
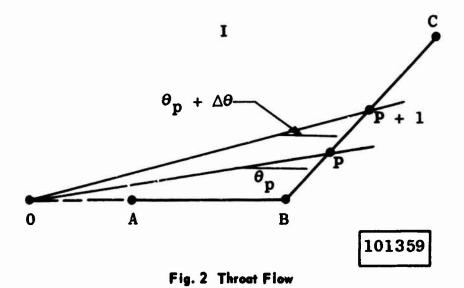


Fig. 1 Major Nozzle Divisions

2.1 THROAT REGION



In calculating flow within the throat region, points A and B of Fig. 2 are given points.

The velocity distribution on AB is given either by an equation or as a series of discrete points. The flow angle at point C, the inflection point, is also an input value. Knowing this angle and the velocity at point B, a left-running characteristic BC (the upstream boundary of the source flow region) can be established using the source flow relation

$$\psi_{\rm p} = \psi_{\rm B} + 2\theta_{\rm p}$$

where the subscript p refers to a point on the characteristic line BC. Line BC is then divided into an arbitrary number of segments having an equal $\Delta\theta$ between successive points. These are initial points for right-running characteristics from line BC. The mass flow in the nozzle is found by integrating along BC using the technique outlined in Section 2.4.

Ar arbitrary number of points are specified as the origin points for the left-running characteristics beginning on the axis. Characteristic lines are calculated until a field point is computed from the last known wall point. As the last characteristic point lies beyond the wall, a mass integration technique is applied to find the wall point location on the characteristic line.

2.2 SOURCE FLOW REGION

The area enclosed by BCD in Fig. 1 consists entirely of source flow, and no characteristic solutions are computed.

2.3 DOWESTREAM REGION

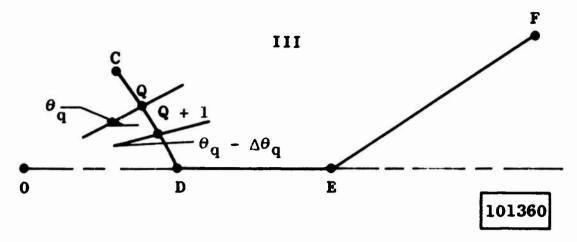


Fig. 3 Downstream Flow

Line CD is a right-running characteristic line on the downstream boundary of the source flow region. This characteristic is calculated in a manner similar to line BC in the throat region. Here the relation used to establish this line is

$$\psi_{\mathbf{q}} = \psi_{\mathbf{c}} + 2(\eta - \theta_{\mathbf{q}})$$

In a manner analogous to that used in defining the axis line AB, it is necessary to designate points D and E and to specify an axial velocity distribution to establish line DE. Also similar to the procedure used for Region I, line DE is divided into an arbitrary number of segments. The axis points are the origins of right-running characteristics.

Successive right-running characteristics originating from line DE are computed, and wall points are found by mass integration as in the throat region.

Line EF in Fig. 3 is a left-running characteristic consisting of uniform parallel flow at the desired design exit Mach number. Line EF is a straight line divided into an arbitrary number of equal intervals for origin points to right-running characteristics. The mass integration along characteristics from line EF is handled in a different manner than integrations beginning on the axis. Here the calculations are performed with an initial mass integration value of

$$m_0 = \left(\frac{r}{r_{\text{oxit}}}\right)^2 X \text{ Total Mass}$$

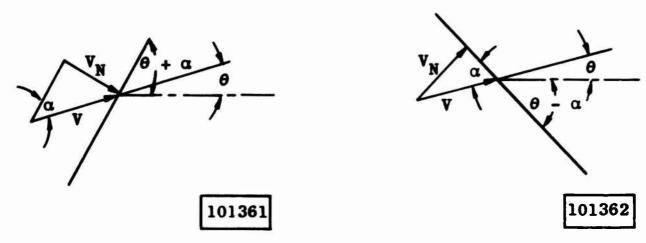
2.4 MASS INTEGRATION TECHNIQUE

The differential equation governing mass flow at a point on a characteristic line is

$$dM = 2\pi \cdot r \cdot V_N \cdot \rho \cdot ds \tag{1}$$

The normal component of velocity at a point on either a right-running or a left-running characteristic is

$$V_N = V \cdot \sin \alpha$$



a. Left-Running

b. Right-Running

Fig. 4 Characteristics

Let
$$\rho = \left(\frac{\rho}{\rho_t}\right) \cdot \rho_t$$
 where $\left(\frac{\rho}{\rho_t}\right) = \left(1 - \overline{W}^2\right)^{\frac{1}{\gamma - 1}}$ and $V = \frac{V}{V_{max}} \cdot V_{max} = \overline{W} \cdot V_{max}$. Now Eq. (1) may be expressed as

$$dM = 2\pi \cdot r \cdot W \cdot V_{max} \cdot \sin \alpha \cdot (1 - W^2)^{\frac{1}{\gamma - 1}} \cdot \rho_t \cdot ds \qquad (2)$$

For a given nozzle condition, the factor $2\pi \cdot V_{max} \cdot \rho_t$ is constant. By letting $m = \frac{M}{2\pi \cdot V_{max} \cdot \rho_t}$ and substituting in Eq. (2), one obtains the nondimensionalized mass differential equation

$$dm = r \cdot W \cdot (1 - W^2)^{\frac{1}{\gamma - 1}} \cdot \sin \alpha \cdot ds \tag{3}$$

By defining

$$r \cdot W \cdot (1 - \overline{W}^2)^{\frac{1}{\gamma - 1}} \cdot \sin \alpha = f(s)$$

Eq. (3) can be simplified to

$$dm = f(s) ds (4)$$

To calculate the nondimensional flow in the nozzle, the following technique is used.

In the throat region, the left-running characteristic defining the origin of the source flow region, Region II in Fig. 1, is known from the axis to the wall. Equation (4) is integrated as follows:

For each point on the line BC, the value f(s) is calculated. The distance (s) from the axis to any point is the sum of the straight line segments from point to point.

The mass integral is computed by analytically evaluating a parabolic fit through each three consecutive points and summing the integral values. The limit of integration of each integral is from the first to the second point.

Computations for mass in the downstream region, Region III in Fig. 1, is carried out in a similar form except that integration is along the right-running characteristic line CD.

2.5 LOCATING WALL POINTS ON A CHARACTERISTIC

The final point calculated on each characteristic line will be beyond the corresponding wall point for that line. Hence, if the nondimensionalized mass flow is integrated to the final point it will exceed the nozzle mass flow. To find the unknown wall point, the sum of the mass flow from point to point is calculated until a point on the characteristic line is reached where the line mass integral exceeds the known nozzle mass flow. An iteration technique is applied to find the unknown wall point. The values of the wall point are calculated by linear interpolation of the known end point values.

3.0 RESULTS

A comparison of theoretical results and the characteristic solution in the transonic region is shown in Fig. 5. The points shown were calculated by the program included in this report.

One important factor in the proper use of this program is the selection of the initial points of the characteristic line beginning on the axis. The spacing will depend upon the axis velocity distribution. It has been found that a value of $1.5 \stackrel{<}{\sim} p \stackrel{<}{\sim} 2.0$ will result in a good spacing in the throat where

 X_i = Abscissa at Mach number 1.0

X, = Abscissa at the beginning of source flow region

 $N = Nth point 1 \le N \le M$

M = Total number of points on the throat axis

X = Abscissa corresponding to the Nth point

$$\frac{X - X_1}{X_2 - X_1} = \left(\frac{N - 1}{M - 1}\right)^p$$

A prior computer program was written to obtain the inviscid wall contours by means of an extrapolation technique based on the starting known wall point and extending this along the wall streamline by extrapolation of the flow direction. The technique was found to be unsatisfactory since errors tended to be propagated from point to point. It was also found that the network size greatly affected the accuracy in locating the wall. With the mass flow integration technique used, no propagated error occurs since the calculation of each wall point is based on a single characteristic line. The total number of points needed in the characteristic field to obtain satisfactory inviscid wall contours was considerably less than required with the streamline extrapolation technique.

4.0 CONCLUSION

A comparison was made of the flow field in the throat region calculated by the techniques in this report to analytical results of other sources. Excellent agreement of results was found between the methods (see Fig. 5).

With this program an inviscid wall contour can be designed with an initial wall point on the left-running characteristic corresponding to Mach 1.0 on the axis to an exit having uniform parallel flow. It must be kept in mind that the methods applied hold for a perfect gas and that the axis velocity distribution must be specified.

O Characteristic Points from Program

 Δ V/V from Program

-- Ref. 2

-- Ref. 3

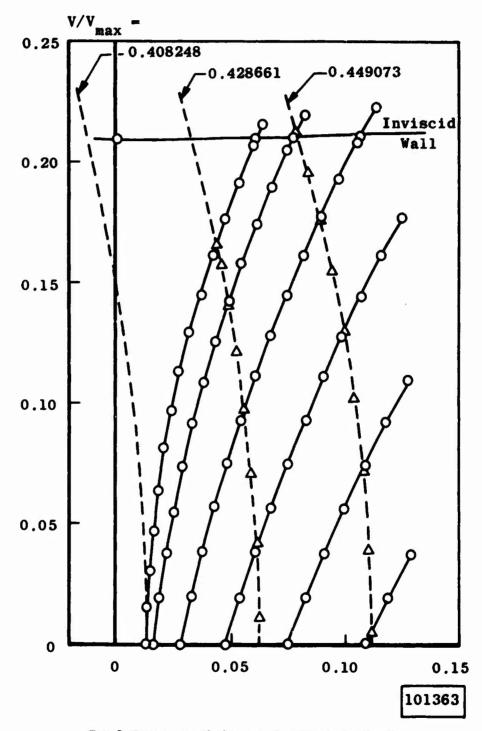


Fig. 5 Comparison of Theoretical and Computed Results

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- 1. Shapiro, Ascher H. The Dynamics and Thermodynamics of Compressible Fluid Flow. The Ronald Press Company, New York, 1953. (2 volumes)
- 2. Sauer, R. "General Characteristics of the Flow Through Nozzles at Near Critical Speeds." NACA-TM-1147, June 1947.
- 3. Oswatitsch, K. and Rothstein, W. "Flow Pattern in a Converging Diverging Nozzle". NACA-TM-1215, March 1949.

APPENDIX !

COMPUTER PROGRAM FOR NOZZLE CONTOUR

The program presented here is based on the methods outlined in the preceding sections. As previously pointed out, there is a difference in the manner of computing the throat and downstream regions, and they may be computed either separately or together.

In either case, a complete set of input data must be prepared for the region under consideration. However, if the downstream region is computed immediately after the throat region, the X-location of the inflection point need not be specified as it is calculated as the wall point on line BC in Fig. 1.

Care must be exercised in specifying the distance between points on the axis to ensure that the characteristic points to be computed will be properly spaced. If axis points A1 and B1 in Fig. 6 are chosen judiciously, A2 will be computed in a manner to make it almost equidistant from its parent points. This effect will be propagated throughout the field.

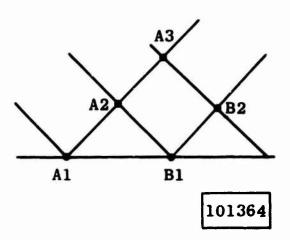


Fig. 6 Axis Distribution

The number of points on an initial characteristic line in either region should be chosen such that the dimension size in the program is not exceeded as points are added to successive characteristic lines.

NOMENCLATURE OF PROGRAM

A	Parameters associated with right-running characteristics				
В	Parameters associated with left-running characteristics				
C	Coefficients of polynomial describing the axis				
S	Characteristic arc length				
FS	Integrand value used in mass integration technique				
AXIS	Refers to parameters located on the centerline				
BEGIN	Refers to parameters on the initially calculated characteristic, i.e., line BC in the throat region and CD in the downstream region.				
FINAL	Refers to the parameters calculated at points along line EF.				
WALL	Refers to the values calculated at the wall points found by the method described in Section 2.5.				
IEND	Control to end program or to calculate				
M	Number of points taken on BEGIN line, BC or CD				
N	Number of axis points				
IX Control dependent on method used to set		dependent on method used to set up axis			
	IX = -1	if discrete X-coordinates are to be read in preceded by the corresponding values of $V/V_{\mbox{max}}$; coefficients, C, not used.			
	IX = 0	if discrete X-coordinates are to be read in and $V/V_{\mbox{max}}$ is to be calculated from the coefficients, C.			
	IX = +1	if axis points are to be computed. Coefficients are to be read in.			
IWOT	Control on amount of calculated points to be written out.				
	IWOT = 0	writes out wall, axis, and first and last characteristics			
	IWOT # 0 writes out all calculated points				
IP Indicat		s which region is to be computed			
	IP = 0	for Region I			
	IP ≠ 0	for Region III			
NP	NP Number of points to be taken on line EF				

GAM Ratio of specific heats

ETA Angle at inflection point, point C, in degrees

XC X-coordinate at point C

X1 & X2 V/V_{max} is a polynomial dependent on an X_R relative to source flow such that

$$V/V_{max} = W = f(\bar{X})$$

where

C

$$\bar{X} = \frac{X_R - X_1}{X_2 - X_1}$$

P Governs distribution on axis. P = 1 for linear distribution. P > 1 packs axis points toward low end of axis.

Constants used in defining the velocity ratio along the axis

in terms of V/V_{max}.

XHI Maximum X-coordinate on the axis, point B or E

XLO Minimum X-coordinate on the axis, point A or D

AXIS(1, N) Axis coordinates to be read in when IX \neq 0

AXIS(3, N) V/V_{max} corresponding to axis points to be read in when IX = -1

Subscripts (on A, B, AXIS, BEGIN, FINAL, and WALL)

First subscript (1-6) 1 = X-coordinate

2 = Y-coordinate

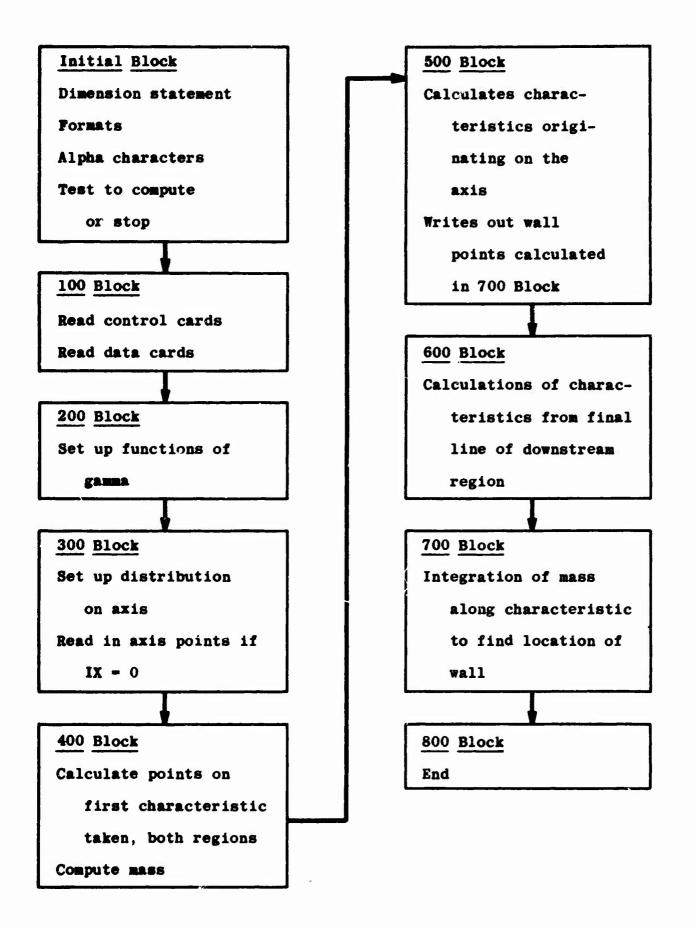
 $3 = V/V_{max}$

4 = Mach angle

5 = Flow angle

6 = Mach number

Second subscript (1-100) designates point number.



INPUT DATA AND SAMPLE VALUES

(Input values of IEND, M, N, IX, IWOT, IP, NP, GAM, ETA, XA, X1, X2, P, C, XHI, XLD, and AXIS discussed in Nomenclature of Program.)

Sample input used for design criteria of Mach 8, nozzle half angle, ETA = 12 deg.

Throat region (Region 1):

IEND = 1 (to proceed with calculations)

M = 15 (15 right-running characteristics from line BC)

N = 20 (20 axis points right-running characteristics)

IX = 1 (to calculate distribution along axis)

IWOT = 1 (to write out all characteristics)

IP = 0 (to calculate in the throat region)

NP = 0 (to calculate in the throat region)

GAM = 1.4

ETA = 12 deg

XC = 0.0 (not used for throat calculations)

X1 = 0.4727 (discussed in Nomenclature of Program)

X2 = 1.91607 (discussed in Nomenclature of Program)

P = 2.0 (square distribution on axis)

C(1) = 0.408248247

C(2) = 0.551273121

C(3) = 0.010438091

C(4) = -0.369697773

C(5) = 0.229213428

C(6) = -0.042703583

XHI = 1.91607

XLO = 0.4727

Downstream Region (Region III):

IEND = 1

M = 40

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N = 6

IX = 1

IWOT = 1

IP = 1

NP = 35

GAM = 1.4

ETA = 12 deg

XC = 0.0 (calculated in throat region and not necessary to read in)

X1 = 13.015491

X2 = 15.211972

P = 1.0

C(1) = 0.961279408

C(2) = 0.005421945

C(3) = 0.005421945

C(4) = 0.001807315

C(5) = 0.0

C(6) = 0.0

XHI = 15.211972

XLO = 13.015491

IEND = 0 (to end program).

```
C
         05314 MAIN PROGRAM AXI-SYMMETRIC SUPERSONIC NOZZLE
         PROGRAMMED BY WC MOGER AND DB RAMSAY
C
         COMPUTATION BASED ON MASS FLOW INTEGRATION BY PARABOLIC FIT
C
C
         DIMENSION A(6.100).B(6.100). C(6) .D(10).FS(100).S(100)
         DIMENSION AXIS(6+100) + BEGIN(6+100) + FINAL(6+100) + WALL(6+100)
         EQUIVALENCE (BEGIN(1) + FINAL(1))
         FORMAT (9H PN 05314)
     1
     2 0 FORMAT (11.78H
     2 1
                                     )
     3
         FORMAT (1615)
         FORMAT (6E12.0)
         FORMAT (////10X.5HINPUT///5X.
       1 45HNUMBER OF POINTS ON FIRST CHARACTERISTIC (M)=13//
       2 5X.29HNUMBER OF POINTS ON AXIS (N)=13//5X.6HGAMMA=F7.4//
       3 5X+23HINFLECTION ANGLE (ETA)=F7.3+2X+7HDEGREES//
       4 5X+36HCOORDINATE OF INFLECTION POINT (XC)=F9.5//
       5 5X.38HFACTORS IN V/VMAX TO DETERMINE X (X1)=F9.5//38X
       6 5H(X2)=F9.5//5X.38HPOWER GOVERNING AXIS DISTRIBUTION (P)=F8.5
       7 //5X+31HCOEFFICIENTS IN TERMS OF V/VMAX//10X+5HC(1)=1PE13.7
       8 //10X+5HC(2)=1PE13+7//10X+5HC(3)=1PE13+7//10X+5HC(4)=1PE13+7
       9 //10X+5HC(5)=1PE13.7//10X+5HC(6)=1PE13.7)
     7 0 FORMAT (1H1+10X+A5//10X+5HPOINT+8X+1HX+14X+1HY+12X+6HV/V-AX
     7 1 6X+12HMACH ANG.(D)+3X+12HFLOW ANG.(D)+4X8HMACH NO.//10(10X
     7 2 •13•2X•1P6E15•7/1/1
     8 0 FORMAT(1H110XA5+I3//10X+5HPOINT+8X+1HX+14X+1HY+12X+6HV/VMAX
       1 6X+12HMACH ANG.(D)+3X+12HFLOW ANG.(D)+4X8HMACH NO.//)
         FORMAT (10X+13+2X+1P6E15+7)
    10
         FORMAT (1CHOFELD LINE . 13.6H POINT . 13)
    11
         FORMAT (10x+13+2x+1P6E15.7+2x+6H(MASS))
C
    15
         TYPE 1
         WRITE OUTPUT TAPE 24.1
         XXC=1.0
         IFIRS = 6669798283
         IAXIS = 61876982
         ICHAR = 63686179
         IWALL = 86617373
         CONV = 57.29578
    17
         READ 2+IEND
         IF(IEND)100,804,100
   100
         DO 101 J=1,600
         AXIS(J)=0.0
   101
         0.0=(L)A
         SENSE LIGHT 0
         WRITE OUTPUT TAPE 24+2+IEND
         READ 3+M+N+IX+IWOT+IP+NP
         READ 4.GAM.ETA.XC.X1.X2.P
         READ 4.C
         WRITE OUTPUT TAPE 24,5,M.N.GAM.ETA,XC.X1,X2,P.(C(J),J=1,6)
         ETA=ETA/CONV
         IF(XC)200,103,200
   103
         XC=XXC
```

```
C
C
          200 SERIES SETS UP FUNCTIONS OF GAMMA USED THROUGHOUT
C
                     THE PROGRAM
   200
         G9 = 2.0/(GAM-1.0)
          G8 = 1.0/G9
          G7 = GAM+1.0
          G6 = GAM-1.0
         G5 = G6/G7
         G4 = SQRTF(G5)
         G2 = 1.0/G4
         G1 = 1.0/G6
         EXP
               = 0.5/G5
         CONST = (0.5*G7)**EXP
         EXP
                = -EXP
         NN=1
C
         300 SERIES SETS UP DISTRIBUTION ON THE AXIS
C
   300
         IF(IX)310,305,301
   301
         READ 4.XHI.XLO
         DX=XHI-XLO
         FN = FLOATF(N-1)
         DO 304 J=1.N
          IF(IP)303+302+303
   302
         K#J
         GO TO 304
   303
         K=N-J+1
   304
         AXIS(1.K)=DX*(FLOATF(N-J)/FN)**P+XLO
         GO TO 306
   316
         READ 4.(AXIS(3.J).J=1.N)
   305
         READ 4.(AXIS(1.J).J=1.N)
   306
         DO 307 J=1.N
         X=AXIS(1.J)
         X = (X - X1) / (X2 - X1)
         IF(IX)311,312,312
         W=AXIS(3+J)
   311
         GO TO 313
   312
         W=C(1)+X*(C(2)+X*(C(3)+X*(C(4)+X*(C(5)+X*C(6)))))
         AXIS(3,J)=W
   313
         WW
         XM
                    = SQRTF(G9*WW/(1.0-WW))
         AXIS(6.J) = XM
         S(J)=1.0/XM
         AXIS(4.J) = ASINF(S(J)) + CONV
   307
         WRITE OUTPUT TAPE 24.7.IAXIS.(K.(AXIS(J.K).J=1.6).K=1.N)
         CM=AXIS(6+N)
         DO 308 J=1+N
   308
         AXIS(4,J)=S(J)
         IF(IP)309,400,309
   309
         XM=COSRF(ETA)/XC
         XM=XM*XM
         XM=FMA(XM+GAM)
         AXIS(6)=XM
```

```
c
         400 SERIES SETS UP FIRST CHARACTERISTIC AND
C
                     COMPUTES MASS
   400
         PO=G2*ATANF(SQRTF(G5*(AXIS(6)*AXIS(6)-1.0)))
       1 -1.5707963+ASINF(1.0/AXIS(6))
         EM = ETA/FLOATF(M-1)
         DO 401 J=1.M
            = FLOATF(J-1) *EM
         IF(IP) 403, 402, 403
   402
         XM=FMV(PO+T+T+GAM)
         GO TO 404
   403
         T=ETA-T
   409
         XM=FMV(PO+2.0*FLOATF(J-1)*EM.GAM)
   404
         W=XM+XM+G8
         R = SQRTF(1.0/(CONST+XM+((1.0+G8+XM+XM)++EXP)))
         IF(IP)406,405,406
   405
         K=J
         GO TO 407
   406
         K=M-J+1
   407
         A(1+K)=R*COSRF(T)
         A(2*K)=R*SINRF(T)
         A(3.K)=SQRTF(W/(1.U+W))
         A(4,K)=1.0/XM
         A(5,K)=T
   401
         A(6,K)=XM
   410
         IEND = 6*M
         DO 411 J=1.IEND
         BEGIN(J) = A(J)
   411
         BEGIN(2,1)=0.0
         BEGIN(5,1)=0.0
   420
         DO 421 J=1.6
         WALL(J) = A(J_M)
   421
         5(1)=0.0
   430
         DO 431 J=2.M
               = A(3,J)
         DX = A(1+J) - A(1+J-1)
         DY = A(2 + J) - A(2 + J - 1)
         S(J)=S(J-1)+SQRTF(DX+DX+DY+DY)
   431
         FS(J)=A(2,J)*W*A(4,J)*(1.0-W*W)**G1
   440
         LAST = M - 2
         SUM = 0.0
         DO 441 J=1.LAST
         K = J
         CALL PARAB(S(K) +FS(K) +D(1))
   441
         SUM=POLNT(D(1)+S(K)+S(K+1))+SUM
         SUM=POLNT(D(1)+S(LAST+1)+S(LAST+2))+SUM
         XMASS = SUM
         DO 451 J=1.M
   460
         BEGIN(4,J) = ASINF(BEGIN(4,J)) +CONV
         BEGIN(5+J) = BEGIN(5+J)*CONV
   461
         WRITE OUTPUT TAPE 24,7,1FIRS +(K+(BEGIN(J+K),J=1,6),K=1,M)
   470
         LAST = M
         LINE = 2
```

C

```
C
         500 SERIES COMPUTES CHARACTERISTICS ORIGINATING
                     ON THE AXIS
   500
         DO 501 J=1.6
   501
         B(J) = AXIS(J.LINE)
   502
         DO 506 J=1.LAST
         K = J
         IF(IP)504,503,504
   503
         CALL OFELD(A(1+K)+B(1+K)+B(1+K+1)+G9)
         GO TO 505
   504
         CALL OFELD(B(1+K)+A(1+K)+B(1+K+1)+G9)
   505
         B(6,K+1)=1.0/B(4,K+1)
         IF(SENSE LIGHT 1)507,506
   506
         CONTINUE
         GO TO 508
   507
         TYPE 10.LINE.J
         LAST = J
         SENSE LIGHT 1
   508
         LASTP=LAST+1
         IGO=1
         ME=LINE
         IF(IP)509,700,509
   509
         FINAL (6+NN) =0.0
         GO TO 700
   538
         IF (N-LINE) 539,550,539
   539
         LINE=LINE+1
         DO 540 I=1.600
   540
         A(I)=B(I)
         GO TO 500
         DO 542 J=1.LINE
   541
         WALL(4,J) = ASINF(WALL(4,J))*CONV
   542
         WALL(5,J)=WALL(5,J)*CONV
         I=6#LINE
         DO 543 JJ=1+I
   543
         B(JJ)=WALL(JJ)
         JJ=LINE
         DO 545 L=1.LINE
         DO 544 I=1.6
   544
         WALL(I,L)=B(I,JJ)
   545
         JJ=JJ-1
         WRITE OUTPUT TAPE 24.7. IWALL, (K, (WALL, J, K), J=1.6), K=1.LINE)
         XXC=WALL(1.K)
         GO TO 800
   550
         IF(IP)600,541,600
C
C
         600 SERIES COMPUTES CHARACTERISTICS ORIGINATING ON
                     THE FINAL LINE OF THE DOWNSTREAM SEGMENT
C
   600
         IF(NN-1)603.601.603
   601
         NNP=N+1
         W=AXIS(3.N)
         FS(NP)=SQRTF(2.0*XMASS/(W*(1.0-W*W)**G1))
         DELX=FS(NP) *SQRTF(CM*CM-1.0)
         FN=1.0/FLOATF(NP-1)
         DO 602 JJ=1.NP
```

```
F=FLOATF(JJ-1)#FN
         FINAL(1+JJ)=AXIS(1+N)+F*DELX
         FINAL(2,JJ)=F*FS(NP)
         FINAL (3.JJ) =W
         FINAL(4,JJ)=AXIS(4,N)
         FINAL (5,JJ) =0.0
   602
         FINAL (6.JJ) = XMASS*F*F
   603
         NN=NN+1
         DO 604 1=1.600
   604
         A(1)=B(1)
         DO 606 J=1,600
   606
         B(J)=FINAL(J)
         DO 607 J=NN+LAST
         K=J
         CALL OFELD(B(1+K)+A(1+K)+B(1+K+1)+G9)
         B(6*K+1)=1*0/B(4*K+1)
         1F(SENSE LIGHT 1)608,607
   607
         CONTINUE
         GO TO 609
   608
         TYPE 10.NN.J
         LAST=J
   609
         LASTP=LAST+1
         IGO=NN
         ME=NNP
         GO TO 700
   640
         NNP=NNP+1
         IF(NN-NP)600,641,600
   641
         NL=NNP-1
         DO 642 J=1.NL
         WALL(4,J)=ASINF(WALL(4,J))+CONV
         WALL(5,J)=WALL(5,J)#CONV
   642
         WRITE OUTPUT TAPE 24,7,1WALL,(K,(WALL(J,K),J=1,6),K=1,NL)
         GO TO 800
C
         700 SERIES WRITES OUT CHARACTERISTICS AND INTEGRATES
C
C
                     ALONG CHARACTERISTIC FOR WALL POINT
   700
         IF((WOT)701,703,701
         WRITE OUTPUT TAPE 24.8.1CHAR.ME
   701
         DO 702 J=IGO+LASTP
         Z = ASINF(B(4*J))*CONV
         T = B(5*J)*CONV
         IF(1GO-J)723,721,723
   721
         IF(1P)722.723.722
   722
         IF(N-ME)724,723,723
   724
         WRITE OUTPUT TAPE 24,11,J,B(1,J),B(2,J),B(3,J),Z,T,B(6,J)
         GO TO 702
         WRITE OUTPUT TAPE 24.9.J.B(1.J).B(2.J).B(3.J).Z.T.B(6.J)
   723
   702
         CONTINUE
         IF(SENSE LIGHT 1)704,705
   703
   704
         IF(IP)641.541.641
   705
         5(1)=0.0
         DO 706 J=2.LASTP
               = B(3.J)
         DX=B(1,J)-B(1,J-1)
```

C

```
DY=B(2+J)-B(2+J-1)
      S(J)=S(J-1)+SQRTF(DX+DX+DY+DY)
706
      FS(J)=B(2,J)*W*B(4,J)*(1.0-W*W)**G1
      IF(IP)708,707,708
707
      SUM=0.0
      GO TO 709
708
      SUM=FINAL (6+NN)
709
      DO 710 J=IGO.LASTP
      K = J
      CALL PARAB(S(K)+FS(K)+D(1))
      ADD=POLNT(D(1),S(K),S(K+1))
      SUM = ADD + SUM
      DEL = XMASS - SUM
      IF(DEL)712,711,710
710
      CONTINUE
      IF(IP)641,541,641
711
      F1=1.0
      F2 = 0.0
      GO TO 717
712
      AREA=ADD+DEL
      K = 0
      XLO=S(J)
      XH1=S(J+1)
713
      K=K+1
      XX=(XLO+XHI)*0.5
      YY=POLNT(D(1)+S(J)+XX)
      TEST=AREA-YY
      IF(TEST)714,716,715
714
      XHI=XX
      IF(K-20)713,716,716
715
      XLO=XX
      IF(K-20)713,716,716
716
      DX=S(J+1)-S(J)
      F1=(XX-S(J))/DX
      F2=(S(J+1)-XX)/DX
717
      DO 718 I=1.5
      B(I+J+1)=B(I+J)*F2+B(I+J+1)*F1
718
      B(6,J+1) = 1.0/B(4,J+1)
      DO 719 K=1.6
719
      WALL(K,ME)=B(K,J+1)
      LAST=J+1
      IF(IP)720.538.720
720
      IF(N-ME)640,600,538
800
      GO TO 17
804
      END FILE 24
807
      STOP 05314
      END
      FUNCTION POLNT(D,Y,X)
      DIMENSION D(3)
      D2 = D(2)*0.5
      D3 = D(3) *0.33333333
      POLNT = (X-Y)*(D(1)+(X+Y)*(D2+D3*X)+D3*Y*Y)
      RETURN
      END
```

APPENDIX II

SUBROUTINES USED

SQRTF calculates square root of the argument

ASINF calculates angle of argument (in radians)

COSRF cosine, in radians

ATANF gives arctan, in radians

SINRF sine, in radians

FMA calculates Mach number as a function of area ratio,

(A/A* or A*/A), and gamma,

e.g., XM = FMA (RR, G)

where RR = area ratio

G = gamma

FMV calculates Mach number as a function of Prandtl-Meyer angle and gamma,

e.g., XM = FMV(R, G)

where R = Prandtl-Meyer angle

G = gamma

PARAB calculates the coefficients, A1, A2, and A3, of a parabolic fit through three points.

YY(1-3) = FUNCTION of XX(1-3)

i.e., $Y = A1 + A2X + A3X^2$

POLNT integrates the area under the parabola $A1 + A2X + A3X^2$.

i. e., $\int_{x_1}^{x_1} (A1 + A2X + A3X^2) dX$

e.g., sum = POLNT (A(L), X_1 , X_2)

OFELD calculates X, Y, V/V_{max}, Mach angle, flow angle, and entropy at the intersection of a left and a right-running characteristic,

e.g., CALL OFELD(A(1, i), B(1, i), B(1, i+1), G)

where A(1, i) = X-coordinate of right-running characteristic

B(1, i) = X-coordinate of left-running characteristic

B(L, i+1) = X-coordinate of intersection

$$G = \frac{2}{\gamma - 1}$$

FUNCTION POLNT(D+Y+X)
DIMENSION D(2)
D2 = D(2)+0.5
D3 = D(3)+0.33333333
POLNT = (X-Y)+(D(1)+(X+Y)+(D2+D3+X)+D3+Y+Y)
RETURN
END

```
FUNCTION FMV
    FUNCTION FMV RETURNS THE MACH NO. AS A FUNCTION OF GAMMA P.M. ANG
    FUNCTION FMV(R+G)
     A=SQRTF((G+1.0)/(G-1.0))
    B=1.0/A
    P1=4.898979
     R1=A* ATANF(B*P1)- ATANF(P1)
     IF(R-R1)1.10.2
 1
    P2=2.828427
    GO TO 3
 2
    P2=8.944272
     R2=A* ATANF(B*P2) - ATANF(P2)
 3
     IF(R2-R)4,11,4
     P3=P1+(R-R1)+(P1-P2)/(R1-R2)
     IF(P3-1.0)14,15,15
14
    P3=1.0
     IF(ABSF(P2-P3)-0.0005)12.12.5
15
 5
     R3=A* ATANF(B*P3) - ATANF(P3)
     P1=P2+(R-R2)*(P2-P3)/(R2-R3)
     IF(P1-1.0)16,17,17
16
    P1=1.0
17
     IF(ABSF(P3-P1)-0.0005)10,10,6
     R1=A* ATANF(B*P1) - ATANF(P1)
 6
     P2=P3+(R-R3)*(P3-P1)/(R3-R1)
     IF(P2-1.0)18,19,19
18
    P2=1.0
19
     IF(ABSF(P1-P2)-0.0005)11.11.3
10
     FMV=SQRTF(P1**2+1.0)
     RETURN
    FMV=SQRTF(P2**2+1.0)
11
     RETURN
     FMV=SQRTF(P3##2+1.0)
12
     RETURN
```

END

```
SUBROUTINE PARAB
C
         SUBROUTINE PARAB(XX+YY+A)
C
         SUBROUTINE PARAB RETURNS THE COEFFICIENTS A OF A PARABOLIC FIT
C
C
         THROUGH THREE POINTS YY(1-3) = FUNCTION OF XX(1-3)
C
         DIMENSION XX(3)+YY(3)+A(3)
         X1 = XX(1)
         X2 = XX(2)
         X3 = XX(3)
         F1 = X1 - X2
         F2 = X2 - X3
         F3 = X3 - X1
         D = -1.0/(F1*F2*F3)
         Y1 = YY(1) +F2
         Y2 = YY(2) + F3
         Y3 = YY(3) *F1
         A(1) = D*(Y1*X2*X3 + Y2*X1*X3 + Y3*X1*X2)
         A(2) = -D*(Y1*(X2+X3) + Y2*(X1+X3) + Y3*(X1+X2))
         A(3) = D*(Y1+Y2+Y3)
         RETURN
         END
```

FUNCTION FMA(RR,G)

FUNCTION FMA RETURNS THE MACH NO. AS A FUNCTION OF AREA RATIO RR= AREA RATIO (A/A+ OR A+/A) AND G=GAMMA

```
IF(RR - 1.0)20,21,22
20
     R = RR
     GO TO 23
21
     FMA = 1.0
     RETURN
22
     R = 1.0/RR
23
     CONTINUE
     IF(G-GAMMA)1+2+1
 1
     GAMMA=G
     C1=(G+1.0)/(2.0*(G-1.0))
     C2=((G+1.0)+0.5)++C1
     C3=0.5*(G-1.0)
 2
     P1=5.0
     R1=C2*P1/(1.0+C3*P1*P1)**C1
     IF(R1-R)3,10,4
 3
     P2=3.0
     GO TO 5
     P2=9.0
     R2=C2*P2/(1.0+C3*P2*P2)**C1
     IF(R2-R)6,11,6
     P3=P1+(R-R1)+(P1-P2)/(R1-R2)
     IF(P3-1.0)14.15.15
     P3=1.0
15
     IF(ABSF(P2-P3)-0.0005)12,12,7
     R3=C2*P3/{1.0+C3*P3*P3)**C1
     P1=P2+(R-R2)+(P2-P3)/(R2-R3)
     IF(P1-1.0)16,17,17
16
     P1=1.0
     IF(ABSF(P3-P1)-0.0005)10,10,8
17
     R1=C2#P1/(1.0+C3#P1#P1)##C1
     P2=P3+(R-R3)*(P3-P1)/(R3-R1)
     IF(P2-1.0)18,19,19
18
     P2=1.0
19
     IF(ABSF(P1-P2)-0.0005)11,11,5
10
     FMA=P1
     RETURN
11
     FMA=P2
     RETURN
12
     FMA=P3
     RETURN
     END
```

```
SUBROUTINE OFELD (A.B.C.G)
         DIMENSION A(5)+B(5)+C(5)
         X1 = A(1)
         Y1 = A(2)
         W1 = A(3)
         SA1 = A(4)
         T1 = A(5)
         W13 = W1
C
         X2 = B(1)
         Y2 = B(2)
         W2 = B(3)
         SA2 = B(4)
         T2 # B(5)
         W23 = W2
C
         IF (SENSE SWITCH 4)91,92
         CONTINUE
    91
         WRITE TAPE 12+DASH
         WRITE TAPE 12+(A(J)+J=1+5)
         WRITE TAPE 12+(B(J)+J=1+5)
         WRITE TAPE 12.BLANK
          CONTINUE
    92
          DT = T1 - T2
          DW = W1 - W2
          C3 = 0.0
          I = -1
 C
          ST1 = SINRF(T1)
     20
           HST1= ST1
          CT1 = COSRF(T1)
           HSA1= SA1
          CA1 = SQRTF(1.0 - SA1*SA1)
           HCA1= CA1
          ST2 = SINRF(T2)
           HST2= ST2
          CT2 = COSRF(T2)
           HSA2= SA2
          CA2 = SQRTF(1.0 - SA2#SA2)
           HCA2= CA2
           SINA = ST1+CA1 - CT1+SA1
             SA = SINA
           COSA = CT1*CA1 + ST1*SA1
             CA = COSA
           SINB = ST2+CA2 + CT2+SA2
             SB = SINB
           COSB = CT2+CA2 - ST2+SA2
             CB = COSB
           GO TO 40
  C
           ST3 = SINRF(T3)
      30
           CT3 = COSRF(T3)
           CA3 = SQRTF(1.0 - SA3#SA3)
            H1 = ST3*CA3
            H2 = CT3#SA3
```

```
H3 = CT3*CA3
          H4 = ST3*SA3
         SINA = (SA + H1-H2)*0.5
         COSA = (CA + H3+H4)*0.5
         SINB = (SB + H1+H2)*0.5
         COSB = (CB + H3-H4)*0.5
              = (HST1 + ST3)*0.5
         ST1
              = (HSA1 + SA3) + 0.5
         SAI
              = (HCA1 + CA3)*0.5
         CA1
              = (HST2 + ST3) #0.5
         ST2
         SAZ
              = (HSA2 + SA3)*0.5
         CA2
              = (HCA2 + CA3)*0.5
         W13
              = (W1 + W3) * 0.5
         W23
             = (W2 + W3)*0.5
         C3
              = W3
C
    40
         CONTINUE
         E = SINA*COSB
            = COSA*SINB
         D = F - E
         X3 = (F*X2 - E*X1 + COSA*COSB*(Y1-Y2))/D
         Y3 = (F*Y1 - E*Y2 + SINA*SINB*(X2-X1))/D
C
         DX = X3 - X1
         DY = Y3 - Y1
         IF(ABSF(DX) - ABSF(DY))41+42+42
    41
         P1 = DY/SINA
         GO TO 43
    42
         P1 = DX/COSA
         DX = X3 - X2
    43
         DY = Y3 - Y2
         IF(ABSF(DX) - ABSF(DY))44,45,45
    44
         P2 = DY/SINB
         GO TO 45
         P2 = DX/COSB
    45
         P1 = ST1*SA1*P1*2.0/(Y1+Y3)
         P2 = ST2 + SA2 + P2 + 2 \cdot U / (Y2 + Y3)
    50
            = CA1/(SA1*W13)
         Q1
         Q2 = CA2/(SA2+W23)
             = Q2 + Q1
         Q
C
         T3 = (Q2*(P1 + T1 + Q1*DW) + Q1*(T2-P2))/Q
         W3
             = (P1+P2 + Q1+W1 + Q2+W2 + DT)/Q
             = W3*W3
         WW
         SA3 = SQRTF((1.0 - WW)/(G#WW))
C
         I = I + 1
         IF!SENSE SWITCH 4193.94
    93
         CONTINUE
         WRITE TAPE 12.P1.P2.Q1.Q2
         WRITE TAPE 12.X3.Y3.W3.SA3.T3
    94
         CONTINUE
         IF(1)52,51,52
    51
         TOLD = T3
         T3
              = (T3 + (T1+T2)*0.5)*0.5
```

```
GO TO 30
C
       IF(ABSF(T3-TOLD) - 0.00001)60.60.61
    52
       IF(ABSF(C3-W3) - 0.00001)70,70,61
    60
         IF(1-40)62.63.62
    61
    62
         TEMP = T3
         T3 = (T3 + TOLD)+0.5
         TOLD = TEMP
         GO TO 30
C
         SENSE LIGHT 1
    63
    70
         C(1) = X3
         C(2) = Y3
         C(3) = W3
         C(4) = SA3
         C(5) = T3
    80
         RETURN
         DASH = DASH
         BLANK = BLANK
         END
```

APPENDIX III

FIELD POINT CALCULATION

The partial differential equations for supersonic, axially symmetric, irrotational flow are reduced to the following ordinary differential equations by the method of characteristics (Ref. 1):

1.
$$\frac{dY}{dX} = \tan (\theta - a)$$
 (right-running)

2.
$$\frac{dY}{dX} = \tan (\theta + a)$$
 (left-running)

3.
$$d\theta + \frac{\cot a}{W} (dW) - \frac{\sin \theta \sin a}{\sin (\theta + a)} \frac{dY}{Y} = 0$$
 (right-running)

4.
$$d\theta - \frac{\cot \alpha}{W} (dW) + \frac{\sin \theta \sin \alpha}{\sin (\theta + \alpha)} \frac{dY}{Y} = 0$$
 (left-running)

Equations (1-4) are solved by finite difference methods in the following form:

1.
$$\frac{Y_c - Y_a}{X_c - X_a} = \frac{\sin(\theta - a)}{\cos(\theta - a)}$$

2.
$$\frac{Y_c - Y_b}{X_c - X_a} = \frac{\sin (\theta + a)}{\cos (\theta + a)}$$

1.
$$X_c \cdot \sin(\theta - \alpha) - Y_c \cdot \cos(\theta - \alpha) = X_a \cdot \sin(\theta - \alpha) - Y_a \cdot \cos(\theta - \alpha)$$

2.
$$X_c \cdot \sin(\theta + a) - Y_c \cdot \cos(\theta + a) = X_b \cdot \sin(\theta + a) - Y_b \cdot \cos(\theta + a)$$

Solving the system Eqs. (1) and (2), we have

$$X_{c} = \frac{\begin{vmatrix} X_{a} \cdot \sin(\theta - a) - Y_{a} \cdot \cos(\theta - a) - \cos(\theta - a) \\ X_{b} \cdot \sin(\theta + a) - Y_{b} \cdot \cos(\theta + a) - \cos(\theta + a) \end{vmatrix}}{\begin{vmatrix} \sin(\theta - a) - \cos(\theta - a) \\ \sin(\theta + a) - \cos(\theta + a) \end{vmatrix}}$$

$$Y_{c} = \frac{\begin{vmatrix} \sin(\theta - a) & X_{a} \cdot \sin(\theta - a) - Y_{a} \cdot \cos(\theta - a) \\ \sin(\theta + a) & X_{b} \cdot \sin(\theta + a) - Y_{b} \cdot \cos(\theta + a) \end{vmatrix}}{\begin{vmatrix} \sin(\theta + a) - \cos(\theta - a) \\ \sin(\theta + a) - \cos(\theta + a) \end{vmatrix}}$$

3.
$$\theta_c - \theta_a + \frac{\cot a}{W} (W_c - W_a) - \frac{\sin \theta \sin a}{\sin (\theta - a)} \cdot \frac{dY}{Y} = 0$$

4.
$$\theta_c - \theta_b - \frac{\cot \alpha}{W} (W_c - W_b) + \frac{\sin \theta \sin \alpha}{\sin (\theta + \alpha)} \cdot \frac{dY}{Y} = 0$$

APPENDIX IV

DATA PRESENTATION

This appendix given a sample of the output obtained by the methods previously outlined. For each of the two principle sections, there is given a page of wall points, a page of axis points, and several pages of characteristic lines including the first and last characteristics in the respective regions.

As indicated in Section 2.3, each characteristic originating on line EF has an initial mass integration value which is computed at the first point of that characteristic. This initial value of mass appears in the output as the first value in column seven.

SAMPLE CALCULATIONS THROAT REGION

INPUT

NUMBER CF PCINTS CN FIRST CHARACTERISTIC (M) = 15

NUMBER OF POINTS ON AXIS (N) = 20

GAPMA= 1.4000

INFLECTION ANGLE (ETA) = 12.000 DEGREES

CCCRDINATE CF INFLECTION POINT (XC)= .00000

FACTORS IN V/VMAX TC CETERMINE X (X1) = .47270

(x2) = 1.91607

PCWER GOVERNING AXIS DISTRIBUTION (P)= 2.00000

CCEFFICIENTS IN TERMS OF V/VMAX

C(1) = 4.0824825-01

C(2) = 5.5127312-01

C(3) = 1.0438091-02

C(4) = -3.6969777 - 01

C(5) = 2.2921343-01

C(6) = -4.2703583 - 02

FLOW ANG. (D) MACH NO.	.0000000+00 2.8502078+00 .0000000+00 2.6814859+00 .0000000+00 2.5100827+00 .0000000+00 2.3394283+00 .0000000+00 2.1732175+00 2.1732175+00 .0000000+00 1.8660831+00 .0000000+00 1.7290779+00 .0000000+00 1.4925681+00	.0CC0000+00 1.3933238+00 .0000000+00 1.3064451+0C .00000000+00 1.2314991+0C .00000000+00 1.153606+C0 .0000000+00 1.0731280+0C .0000000+00 1.004937+00 9.999985-01
FLOW A	000000000000000000000000000000000000000	+ + + + + + + + + + + + + + + + + + +
MACH ANG. (D)	2.0539411+01 2.1896281+01 2.3477770+01 2.5306148+01 2.7396609+01 2.9759848+01 3.2403734+01 3.5334078+01 3.8554544+01	4.5865592+01 4.9945788+C1 5.4293611+01 5.8890218+01 6.3710936+01 6.8725887+01 7.39CC841+01 7.9198237+01 8.4578386+01
V/VMAX	7.8677154-01 7.68C1048-01 7.4668756-01 7.2289589-01 6.9695680-01 6.6936527-01 6.4072997-01 6.1171489-01 5.8298770-01	5.2684703-01 5.0446791-01 4.8241846-01 4.6298226-01 4.4635751-01 4.2199273-01 4.0977539-01 4.0977539-01
>	000000000000000000000000000000000000000	000000000000000000000000000000000000000
×	1.9160700+C0 1.7681353+00 1.6281957+00 1.4962527+C0 1.3723068+C0 1.2563578+00 1.1484053+C0 1.0484490+C0 9.5648887-C1 8.7252528-C1	7.9655846-01 7.2858834-01 6.6861469-01 6.1663717-01 5.7265632-01 5.3667210-01 5.0868427-01 4.7669825-01
PCINT	10m4n4rm60	111 112 114 118 119 119 119

CINI	×	>	V/WAX	MACH ANG. (D)	FLCW ANG. (D)	MACH NO.
-	.9161003+C	00000	7.8677156-01	2.0539408+01	.3030000+30	2.8502383+00
7	.9952818+	.945156	7.9549330-01	1.9917231+01	8.5714280-01	2.9354581+00
~	.0801	.225607	8.0402024-01	1.9313122+01	1.7142856+00	3.0236094+00
4	.1711983+	862	8.1235499-01	1.8725836+01	2.5714284+00	3.1148757+60
S	.269	.359429	8.2049928-01	1.8154280+01	3.4285712+00	3.2094815+00
9	.3744160+	.179378	8.2845491-01	1.7597439+01	4.2857140+00	3.3076735+00
7	01910	39241	8.3622333-01	1.7054386+01	5.1428568+00	3.4097186+00
00	.6106818+0	.743936	8.4380591-01	1.6524266+01	5.999991+00	3.5159095+00
0	.7434285+	.299093	8.5120382-01	1.6006292+01	6.8571423+00	3.6265660+00
10	.8873420+C	3.9111700-01	8.5841789-01	1.5499752+01	7.7142849+00	3.7420356+00
		.58	8.6544925-01	1.5003956+01	8.5714280+00	3.8627077+00
12	902040	37046	8.7229867-01	1.4518279+01	9.4285706+03	3.9890.085+60
	.3996408+	.169437	8.7896664-01	1.4042151+01	1.0285713+01	4.1214954+00
	.6028	42	8.8545385-01	1.3575026+01	1.1142856+01	4.2604234+00
	.8256230+	.131611	8.9176084-01	1.3116394+01	1.1999998+01	00+559907.5

FIRST

MACH NO.	1.8660831+00 1.939C988+C0 2.0125469+00 2.0855648+C0 2.157C181+00 2.2258865+C0 2.2916781+00 2.3575798+C0 2.4257743+C0 2.4257743+C0 2.4257743+C0 2.4257743+C0 2.4257743+C0 2.4257743+C0 2.8626810+00 2.8587663+00
FLOW ANG.(D)	.0CCCC00+00 1.0392350+00 2.1012785+00 3.1588559+00 4.1863989+00 5.1605961+00 6.9707354+00 6.9585444+90 7.8456521+00 8.7320510+00 9.6165981+00 1.0499024+01 1.1379360+01 1.2257715+01
MACH ANG. (D)	3.2403734+01 3.1944488+01 2.9793983+01 2.8651865+01 2.6696165+01 2.5696165+01 2.5097745+01 2.5097745+01 2.2007672+01 2.2221154+01 2.2221154+01 2.2221154+01 2.1555119+01 2.0908562+01
V/VMAX	6.4072997-01 6.5515689-01 6.6858048-01 6.8206792-01 7.7549145-01 7.2555748-01 7.2555748-01 7.3527285-01 7.486052-01 7.5429984-01 7.5429984-01 7.5429984-01 7.5429984-01
> -	.COCCOOO+CO 3.2461364-02 6.3743327-C2 9.3751433-02 1.2247372-01 1.5061C28-01 1.7651203-01 2.3236074-01 2.3236074-01 2.9620383-01 3.9666738-01 3.6966738-01 4.1062422-01
×	1.1484053+00 1.1998655+00 1.2499484+C0 1.2982467+C0 1.3445549+C0 1.3489131+C0 1.4747146+C0 1.5206479+00 1.5206479+00 1.5206479+00 1.5206479+00 1.5206479+00 1.5206479+00 1.5494731+C0 1.6767485+C0 1.7986778+C0
PCINT	10m450+86010m45

CHAR 14

PCINT	×	>	V/VMAX	MACH ANG. (D)	FLOW ANG. (D)	MACH NG.
-	6.1663717-61	00+0000000	4.6298226-01	5.8890218+01	90+0093006*	1-1679802+60
2	6.4129981-61	3.9233619-02	4.73C1281-C1	5.6408236+01	3.8496754-01	1.2004790+00
٣	6.6711163-01	7.7243581-02	4.8398893-01	5.3957683+01	8.8622018-01	1.2367319+00
4	6.9371605-01	1.1378302-01	4.9594932-01	5.1537991+01	1.5002737+00	1.2771053+03
2	7.2071533-61	1.4862064-01	5.0872992-01	4.9184811+01	2.2261131+00	1.3213150+00
9	7.4767870-C1	1.8156254-01	5.2209978-01	4.6932763+01	3.0553935+00	1.3638263+60
7	7.7415013-61	2.1243068-01	5.3583572-01	4.4803650+01	3.9782077+00	1.4190850+00
œ	7.9974149-01	2.4114160-01	5.4964370-01	4.2821907+01	4.9724523+00	1.4711991+69
σ	8.1794774-01	2.6100686-01	5.5985933-01	4.1442861+01	5.7536622+00	1.5108642+00

MACH NO.	9.999985-01 1.00309064-00 1.0101333+00 1.0209902+00 1.0362937+00 1.0558849+00 1.0796918+00
FLOW ANG. (D)	.00C0C00+00 3.1320498-03 2.8380085-02 9.1275489-02 2.1415192-01 4.1289559-01 7.0198594-01 9.8139678-01
MACH ANG. (D)	.CCOCCOC+CO 8.5501147+01 8.1877508+01 7.8361874+01 7.4791447+01 7.1275463+01 6.7848511+01 6.5401202+01
V/VMAX	4.0824825-01 4.0929893-01 4.11687CC-01 4.1535182-01 4.2048343-01 4.2699439-01 4.3481791-01
>	.000000+00 3.1714399-02 6.6313669-02 1.0166363-01 1.3655434-01 1.7070059-01 2.0385075-01 2.2703553-01
×	4.7270000-C1 4.7394504-01 4.7776127-C1 4.8387963-C1 4.9210774-C1 5.0232067-01 5.1430715-C1 5.2392601-C1
POINT	10m450cm

WALL						
PGINT	×	>	V/VMAX	MACH ANG. (D)	FLOW ANG. (D)	KACH NO.
1	.1659679-0	.0936	4.3637388-01	6.7243410+01	7.6849615-01	1.0844146+00
2	.3236531-0	.6958	4.4267507-01	6.4953063+01	•	1,1037999+00
3	.6188641-0	.1016	4.5446819-01	6.1242553+01	1.3749283+00	1.1406875+00
4	.0159163-0	.11300	4.7022952-01	5.7084779+01	1.9003177+00	1-1912199+00
5	0	2.1325026-01	4.8975707-01	5.2771310+01	2.5526800+00	1.2559231+00
9	.1099133-0	.1638824-0	5.1294391-01	4.8454817+01	3.3308082+00	1.3361250+00
-	.8184284-0	.2106113-0	5.3998546-01	4.4200965+01	4.2770760+00	1.4343556+00
©	.6463544-0	.2805	5.7041743-01	4.0093121+01		1.5527183+00
6	0-6506609.	.3816	-0400141-	3.6169147+01		1.6944240+00
10	.0730759+0	.5248	.3984620-	3.2491226+01		1.8616065+00
11	.2036826+0	2226	6.7621061-01	2.9159999+01	9.1905049+00	2.0523341+00
	.3559671+0	.9841	7.1113326-01	.6241486+0	.0221735+0	2.2616482+00
	.5336236+0	.31763	7.4364038-01	.3708614+0	.0958861+0	2.4870336+09
	.7406534+0	. 72870	7.7338972-01	.1504446+0	.1448058+0	2,7279663+00
15	1.9813879+00	.2	8.0005758-01	•	1.1735549+01	2.9819967+00
	.2602859+0	.80807	8.2381568-01	.7921965+0	.1894637+0	3.2496925+00
	.5812845+0	.4876196-0	8.4459651-01	.6468681+0	.1963565+0	3.5274462+00
	.9477854+0	.26586	8.6272046-01	.5196376+0	.1992298+0	3.8149276+00
	.3614256+0	.14479	8.7832743-01	.4087849+0	1.2003126+01	4.1083057+00
	.8256230+0	.13161	8.9176084-01	.3116394+0	.1999998+0	4+0

INPUT

NUMBER OF POINTS ON FIRST CHARACTERISTIC (M) = 40

NUMBER OF POINTS ON AXIS (N)= 6

GAPMA= 1.4000

INFLECTION ANGLE (ETA) = 12.000 DEGREES

CCORDINATE CF INFLECTION POINT (XC)= .00000

FACTORS IN V/VMAX TO CETERMINE X (X1)= 13.01549

(X2) = 15.21197

PCWER GCVERNING AXIS DISTRIBUTION (P)= 1.00000

CCEFFICIENTS IN TERMS OF V/VMAX

C(1) = 9.6127941-01

C(2) = 5.4219450-03

C(3) = -5.4219450 - 03

C(4) = 1.8073150-03

C(5) = .0000000+00

C(6) = .0000000+00

MACH NO.	7.7999875+00 7.8958308+00 7.9555832+00 7.9867587+00 7.9993301+00
FLOW ANG. (D)	000000000000000000000000000000000000000
HACH ANG. (D)	7.3658990+00 7.2760014+50 7.221C610+00 7.1927242+00 7.1822632+00
V/VMAX	9.6127941-01 9.6216137-01 9.6269634-01 9.6297105-01 9.6307626-01
>	000+00000000000000000000000000000000000
×	1.3015491+01 1.3454787+01 1.3894083+01 1.4333379+01 1.4772675+01
PCINT	

AXIS

PCINT	×	>	V/VMAX	MACH ANG. (D)	FLOW ANG.(D)	MACH NO.
-	.3016149	.000000000	9.6128115-01	.3657298+0	00+000000€	7.8001747+09
7	.249108	6.7080898-02	. 59935	9	3.0769266-01	7.6599080+00
~	.1995820	1.2884605-01	58565	9	6.1538532-01	7.5241795+00
•	.1528195+0	1.6574383-01	57173	0	9.2307741-01	7.3927642+00
5	.1086247+0	2.3818010-01	55758	•	1.2307695+00	7.2654545+00
9	83+0	2.8652272-01		8.0487593+00	1.5384621+00	7.1420527+00
~	.0272348+C	3.3110474-01	52860	9	1.8461542+00	7.0223743+00
6 0	.8972516	3.7222996-01	51376	0	2.1538463+00	6.9062501+00
o	.5415071+0	4.1017423-01	49869	9	2.4615390+00	6.7935175+00
91	.2038263+0	4.4518788-01	48339		2,7692310+00	6.6840221+00
=	046430699	C	0 447840	744421140	C	677
4 (0.000000000000000000000000000000000000	10-340061111		?	0.16360.00	0011101101
71	3+9460816	5-0/32138-01		2	1961949	00+1+81+1+0
<u>.</u>	8.2879571+00	5.3484083-01	9.4361270-01	9.0269773+00	3.6923079+00	6.3735776+00
*	.0117234+0	5.6023427-01	•	9	•0000000•	6.2756842+00
15	.7485398+6	5.8366186-01	7	9	.3076926+	6.1803894+00
16	.4976256+0	6.0527093-01	m	0	4.6153847+00	6.0875878+00
11	.2582455+0	6.2519611-01	ĕ	0	.9230768+	5.9971773+00
18	.0297157+0	6.4356086-01	3	0	5.2307695+00	5.9090594+00
19	.8114152+0	6-6047976-01		9	5384616+	5.8231462+60
20	-6027554+0	6-7405747-01	-	9	8461537+0	00+004662
2			•			
16	341101504	10-1200200	0 2600744-01	1040730401	00463486	007008363737
4 6	11111111	10-11000000	10-41/4670	0.000000		0010000000
77	3+7017717	10-5306/93-01	10-517510-6	.0327978+0	00+8/55/104-0	2.5///854+00
23	.0293494+0	7.1567264-01	9.2636362-01	.0475938+0	6.7692305+00	5.4998669+00
24	.8541614+0	7.2677993-01	9.2451272-01	.0624629+0	7.0769226+00	5.4237622+00
25	.6862394+0	7.3695978-01	9.2263849-01	.0774071+0	7.3846147+00	5.3494029+00
56	.5251775+C	7.4627794-01	9.2074130-01	.0924279+0	7.6923073+00	5.2767284+00
27	.3706380+C	7.5479389-01	9.1882109-01	.1075247+0	7.9999994+00	5.2056761+00
28	2222748+0	7.6256346-01	9.1667789-01	.1227016+0	8.3076915+00	5.1361893+00
59	.0797715+6	7.6963839-01	9.1491166-01	.1379596+0	8-6153842+00	5.0682123+09
8	•	7.7606611-01	9.1292237-01	1.1533003+01	8.9230763+00	5.0016915+00
31	+8111733+C	7.6189167-01	9.1091007-01	1.1687252+01	.230768	2
35	.6845403+0		0887473-0	.1842361+0	9.5384610+00	4.8728262+00
33	.5626840+0		0-6671890	.1998347+0	.8461531+0	4.8103870+00
¥.	.4453752+		0473488-0	.2155227+0	1.0153845+01	4.7492185+00
35	.3323941+0		263036-0	.2313922+0	.9461537+0	4.6892778+00
36	.2235363+C		0050274-0	.2471750+0	.0769230+0	4.6305252+00
37	.1186065+C		9835198-0	2631431+0	.1076922+0	4.5729212+00
38	.0174211+C		9617802-0	2792091+0	1384614+	4-5164281+00
36	9198167+0		9398104-0	2953735+0	1692306+0	4-4610156+00
0		8.1316152-01	8-9176088-01	10+1049116-1	+00000	4.406644400
>	7.54.705.70		2-0000114	0.1460116.	0.444441	• • • • • • • • • • • • • • • • • • • •

FIRST

PCINT	×	>	V/VMAX	MACH ANG. (D)	FLOW ANG. (D)	TACH NO.
-	521107246	00+000000	0-679064	97081		000000000000000000000000000000000000000
. ~	228	2.7676075-02	9.6307944-01	7.1815212+00	1.9201940-03	7.9991533+00
3	.4772961+0	5.5401137-02	.6364273-7	185317	1.3888795-02	3+2676766
4	.4550000+0	8.3298336-02	.6295185-0	194736	4.4776165-02	.9845796+0
S	.4323960+0	1.1156713-01	.6277770-0	212677	1.0471410-01	4
9	.4091433+C	1.4641875-01	.6249137-0	242148	2.0295899-01	.9325416+0
~	.3521563+0	2.2967691-01	.6146759-0	346787	5.2736697-61	•8201662+C
∞ (2981790+0	2.7318902-01	0	465488	8.6439857-01	
6	.2471338+0	3.3135501-01	. 5904732-0	589832	1.1975195+53	.5711426+C
10	.1987605+0	3.8464635-01	.5775403-0	717371	1.5262623+00	.4467588+0
=	.1529877+0	4.3352054-01	.5642314-0	847033	1.8517382+03	.3244619+0
15	.1096250+C	4.783C061-01	.5505993-0	978263	2.1746451+00	0+59
13	.0685220+C	5.1938889-01	9.5366691-01	110193	.4957105+90	7.0877895+60
7	.0295317+0	5.5707946-01	9.5224643-01	244385	.8151419+00	6.9737137+00
15	.9251976+0	5.9165392-31	9.5079955-01	378932	.1332860+90	6.8625117+00
16	.5736241+0	6.2336595-01	9.4932693-01	514368	.4554636+30	6.7541372+00
11	.2394289+6	6.5244726-01	9.4782922-01	650634	.7667773+00	6.6485356+00
81	.9215437+0	6.7910758-31	9.4630711-01	787669	.0823138+00	6.5456536+00
61	.6189686+0	7.0353852-01	9.4476374-31	925463	.3972784+50	6.4453991+03
20	.3307765+C	7.2591481-01	9.4319047-01	063992	.7116784+00	6.3476962+09
71	.0561097+0	7.4639600-01	9.4159648-31	223245	.2256642+03	6.2524587+00
22	. 7941621+C	7.6512852-01	9.3997481-61	343226	.3391525+30	6.1595967+00
23	.5441875+0	7.6224622-01	.3833767-0	483926		6.0690328+00
54	.3054983+€	7.9787,53-01	9.3667330-01	625334	.9652309+03	5.9826934+03
52	.0774452+0	8.1211737-01	9.3498555-01	767472	.2778413+00	5.8944879+20
56	.8594275+6	8.2508722-01	9.3327466-01	910329	.5901749+03	5.8133550+00
27	.6508813+0	8.3687641-01	9.3154062-01	005391	.9022965+00	5.7282029+00
28	.4512890+C	9.4757226-01	9.2978353-01	019823	.2141976+50	5.6479787+00
53	.2601586+0	3.5725562-91	9.2850334-31	034331	.5259473+30	5.5696061+0)
ည	.0770319+0	8.6600107-31	9.2620027-31	°C48912	7.8374,926+03	.4930281+0
31	.9014858+C	8.7387714-01	9.2437429-01	.063579	8.1488550+30	.4181791+0
32	.7331171+6	8.8394737-01	9.2252517-01	.078307	8.4620954+99	. 3449899+3
33	.5715532+0	8.6727034-01	9.2665320-51	93122	8.7712018+30	.2734141+0
34	.4164417+0	8.9290025-01	9.1875831-01	108216	9.0821741+00	.2033936+0
35	.2674540+0	8.9788735-01	9.1644065-01	.122991	9.3930002+00	.1348802+0
36	·1242823+C	9.(227861-01	.1490316-0	138048	9.7037250+00	Ó
37	.9866361+0	9.(611525-01	.1293669-0	.153190	10014391+01	.0021621+0
38	.8542423+0	9.0943893-01	.1095636-0	168417	.0324940+0	.9378617+C
39	.7268463+C	9.1228611-01	.0894115-0	.183731	.7635411+0	ŗ
04	.6042041+C	9.1469119-01	.0696913-0	991334+0	3+16L5+6	131594+0
41	.4862912+0	.1666662-0	-0485428-	.2146252+	256081	.7526752+0
45	22916+0	3003	211650-0	302092+0	66325+0	933866+6
43	.2626013+0	.1956167-0	.067581-	2458868+0	876494+0	.6352371+0
4	.2613418+0	.1957465-0	-1305903-	1.2465784+01	88C418+0	45355+0

INIO	×	>	VVWAX	MACH ANG. (D)	FLOW ANG. (D)	FACH NO.	
~	.5884793+0	4767692-0	-6308672-	7,1807683+00	9	442-0	(MASS)
ı m	.5665007+0			7.1811677+00	-6364993-	9995443+	
*	.5444182+0	-4026169-0	-6305919-	7,1836148+00	.1582197-0	9968338+0	
8	0363+0	.683	.629950	7.1902502+00	7338183	9894934+0	
9	0+28606640	.970	6286096-	7.2040906+00	.0316627-0	9742247	
_	.4752964+0	.266	.6262948-0	7.2279440+00	81749-0	94	
∞	.4164562+0	.982	•	7.3177855+00	.92874	7.8509894+00	
•	.3605111+0	049.	.6070023-0	7.4244874+00	8.3309891-01	7.7387766+00	
20	.3074709+0	.242	-5955826-	7.5390096+30	17499	7.6218844+00	
11	.2571945+0	.793	-5835609-	7.6581923+00	51440	7.5039572+00	
12	.2095151+0	.297	-5710745-	7.7805606+00	.8505884	7.3866487+00	
13	.1642974+0	.759		7.9052844+00	.18403	7.2708305+00	
14	.1213883+0	.181	-5449829-	8.0318834+00	.5151235	7.1569609+00	
15	.0806450+0	.567		8.1599853+00	.84396	7.0453480+00	
16	.0419349+0	.920		8.2894073+00	17101	03+6660986-9	
17	.0051350+0	.2		8.4199901+00	.49651	6.8292879+00	
8	.7012890+C	.539		8.5516363+00	3.8206829+00		
61	3680956+0	-80970608-		8.6842405+00	4.1436195+00		
2	.0507631+0	.056		8.8177695+60	4.4655642+00		
21	.7483522+0	.281	.4445933-	8.9521608+00	4.7865763+00	6.4263337+00	
22	.4599926+C	.486	*	9.0873880+60	5.1067830+90		
23	.1848629+0	.673	4	9.2234379+00	5.4263103+00	6.2388885+00	
24	.9222008+0	.8439	.3978063-	9.3602861+00	5.7452134+30	6.1484703+09	
25	.6713039+0	.998	•	9.4979151+00	6.0635035+00	6.0601763+00	
92	.4315040+6	.1385		9.6363222+00	6.3813008+00	5.9739383+00	
2.2	.2021851+C	.265	9.3488986-01	9.1754937+00	6.6986203+00	5.8896980+00	
28	.9827652+0	.379		9.9154438+00	7.0155250+00	5.8073830+00	
62	.7727101+0	.483	•	1.0056150+01	7.3320183+00	5.7269435+00	
30	.5715111+C	.575		1.0197636+01	3	5.6483092+00	
31	.3786948+0	.658		1.0339884+01	7.9639936+00	5.5714322+00	
32	-1938218+0	.732		1.0482909+01	~	5.4962507+00	
33	.0164728+C	•		٠.	~	5.4227047+00	
34	.8462620+C	85		.0771336+0	š	5.3507447+00	
35	.6828221+0	.906		0+0519160*	$\ddot{\sim}$	5.2803192+00	
36	.5258118+0	.950	7	.1062960+0	-	5.2113857+00	
37	.3749098+0	.988	•	1.1209992+01		5.1438997+00	
38	.2298125+0	.002	9.1519266-01		:01	5.0777881+00	
39	.0902355+0	0	7	1.1506550+01	.0480905+0	5.0133348+00	
ç	.9559124+0	000	9.1131732-01	1.1656109+01	1.0794587+01	4.9495855+00	
11	.8265888+0	.008	.093	.1806528+0	1108080	4.8874044+00	
42	.7020292+	8	.073	1.1957829+01	1421405	4.8264483+00	
£3	820076+C	.01	533569-0	1,2110030+01	.17345	4.7666773+00	
4,	. 5353376+0	2	0451646-	1.2171643+01	.1861999	4.7429096+00	

	(BASS)
MACH NO.	3.9617458-04 7.9997830+00 7.9985890+00 7.9981332+00 7.9182632+00 7.9182632+00 7.8453714+00 7.8453714+00 7.653200+00 7.2099009+00 7.2099009+00 7.2099009+00 7.2099009+00 6.9336068+00 6.9336068+00 6.9336068+00 6.9336068+00 6.9336068+00 6.9336068+00 6.9336068+00
FLOW ANG. (D)	3.000000000000000000000000000000000000
MACH ANG. (D)	7.1807683+00 7.18199528+00 7.1821900+00 7.1819450+00 7.2044750+00 7.2552775+00 7.4609984+00 7.4609984+00 7.5765189+00 7.5765189+00 7.5765189+00 7.5765189+00 7.5765189+00 8.0774645+00 8.1841716+00 8.1841716+00 8.250517+00 8.4020571+00 8.5254090+00 9.2007500+00 9.4372624+00 9.4372624+00
VZVMAX	9.6308672-01 9.6308493-01 9.6307451-01 9.6297859-01 9.6297859-01 9.6295254-01 9.6093284-01 9.6093284-01 9.6093284-01 9.6093284-01 9.5018141-01 9.501806-01 9.5173185-01 9.551990-01 9.551869-01 9.551869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01 9.558869-01
>	7.6290921-01 7.9065502-01 8.1881638-01 8.4796024-01 9.1235510-01 9.9914109-01 1.0821078+00 1.2973871+00 1.2973871+00 1.2973871+00 1.4646644+00 1.4646644+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.5924700+00 1.59249000 1.7966075+00 1.7966075+00
×	2.1267366401 2.0823545401 2.0823545401 2.0345768401 2.0345768401 1.9373260401 1.8681285401 1.8681285401 1.8681285401 1.8681285401 1.6764182401 1.6764182401 1.6764182401 1.6764182401 1.5623855401 1.5623855401 1.3636482401 1.269917401 1.1269917401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401 1.0268272401
PGINT	0126489780010848978010848978

POINT	*	>	V/VMAX	MACH ANG. (D)	FLOW ANG. (D)	MACH NO.	
91	2.6649939+01	1.4410507+69	9.6308672-01	7.1807683+00	00+0000000	1.4135117-03	(MASS)
61	2.6429393+01	1.4688359+00	9.6308516-01	7.1809293+00	6.9260668-04	7.9998092+00	
20	2.6204029+01	1.4972227+00	9.6307722-01	7.1817504+00	4.4034243-03	7.9988993+00	
21	2.5967243+01	1.5270283+00	9.6305423-01	7.1841282+00	1.5088305-02	7.9962660+00	
22	2.5709681+01	1.5593958+00	9.6300389-01	7.1893312+00	3.8319094-02	7.9905091+00	
23	2.5423982+01	1.5955569+00	9.6291017-01	7.1990125+00	8.1213124-02	9798206+00	
54	2.4629440+01	1.0934848+00	9.6252909-01	7.2382704+00	2.5014287-01	7.9367680+09	
25	2.3829899+01	1.7902671+00	10-6966619°6	7.2925438+00	4.7613372-01	7.8780167+00	
92	2.3045732+01	1.8826531+00	9.6137278-01	7.3564206+00	7.3351656-01	7.8099818+00	
27	2.2285487+01	1.9695286+00	9.6067087-01	7.4274484+00	1.0114538+00	7.7357091+00	
82	2.1552441+61	2.0565609+00	9.5990853-01	7.5040214+00	1.3033269+00	7.6572170+00	
62	2.0847808+01	2.12>7404+00	9.5909577-01	7.5850244+00	1.6949362+00	7.5759136+00	
30	2.0171424+Ci	2.1952531+00	9.5823950-01	7.6696790+00	1.9135914+00	7.4927857+00	
31	1.9522790+01	2.2593409+00	9.5734495-01	7.7573925+00	2.2273181+00	7.4085730+00	
32	1.8900998+01	2.3182955+00	9.5641650-01	7.8476769+00	2.5446217+00	7.3238654+00	
33	1.8304995+01	2.3724206+00	9.5545686-01	7.9402130+00	2.8646722+00	7.2390496+00	
4.	1.7733666+61	2.4220187+00	9.5446869-01	8.0347023+00	3.1866429+00	1.1544667+00	
35	1.7185971+01	2.4673768+00	9.5345407-01	8-1309077+00	3.5099629+00	7.0703731+00	
36	1.6833335+01	2.4954010+00	9.5275689-01	8.1965532+00	3.7288582+00	7.0141298+00	

	(MASS)
MACH NO.	3.0569627-03 7.9998692+03 7.996697+03 7.9968147+00 7.9919441+00 7.9464403+00 7.9464403+00 7.9959341+00 7.699341+00
FLOW ANG. (D)	.000000000 7.0704218-64 3.7859675-03 1.2861266-02 3.2666104-02 6.9223334-02 2.1392447-01 4.1230860-01 6.4241042-01 1.1626606+00
MACH ANG. (D)	7.1807683+00 7.1809293+00 7.1816152+60 7.1836320+00 7.1962348+00 7.2294136+00 7.2761469+60 7.3945486:00 7.3945486:00
V/VHAX	9.6308672-01 9.6308516-01 9.6307853-01 9.6301645-01 9.6293706-01 9.6215954-01 9.6032340-01
>	2.1191923+39 2.1470143+00 2.1755822+03 2.2394718+00 2.2778305+00 2.4936320+00 2.5992021+00 2.5992021+00 2.1947293+00
×	3.2032512+01 3.1584878+01 3.1343863+01 3.1343863+01 3.0771034+01 2.907261+01 2.9014527+01 2.8126076+01 2.8126076+01 2.5776019+01
POINT	46.56.26.26.26.26.26.26.26.26.26.26.26.26.26

		(MASS)
	MACH NO.	5.6540474-03 (MASS) 7.9998176+00 7.9991482+00
	MACH ANG. (D) FLOW ANG. (D)	.0000000000 6.9508192-04 3.4167785-03 1.0662936-02
	MACH ANG. (D)	7.18^7683+00 7.1809213+00 7.1815258+00 7.1831312+00
	V/VMAX	9.6308672-01 9.6308523-01 9.6307939-01 9.6306387-01
	>	2.8621315+30 2.949653+00 2.9387374+00 2.9668533+00
40	×	3.8087907+C1 3.7866738+C1 3.7638563+C1 3.7415018+C1
CHAR 40	PCINT	35 34 38

HALL						
PCINT	×	>	V/VMAX	MACH ANG. (D)	FLOW ANG. (D)	MACH NO.
-	.8256243+	8-1316152-01	.9176088-0	+	.1999999	163+0
7	028480+C	8.2948851-01	03-	1.2430792+01	1.1985932+31	4.4518761+00
~	-9884616+C		.9554486-0	000	.1954040	0+696
4	.9881107+C		-9759303-0	+	.1893385	5529632+0
S	.2013489+C		.9974154-0	0+	.1804278	·6299496+C
•	.3279902+C		.^192807-0	9	.1691594	.6697233+0
-	.7743664+C		.0851561-0	+	.1239442	.8616621+9
•	8142+C		.1448422-0	\$.0703148	.0537828+0
•	.8459027+C		.1975869-D	0	.0129364	.2431212+0
01	.4509450+C	•3166665+0	.2438556-9	1.0634692+01	.5430785	.4186893+0
11	0955232+	1.4210430+00	.28450	1.0306948+01	.9591629+3	5
12	.7772609+C	.524891	3202331-	1.0013970+01	8.3879515+30	.7538191
<u> </u>	.4935469+0	1.6268757+00	-3518756-	O	.8334778+3	.9246984+9
<u>*</u>	.2429228+C	1.7263847+00	. 3400468-	C	.2983612+0	.0511369+0
<u>~</u>	.0024924+0	1.6228512+00	.4052538-	Ç	. 7838965+0	.1956122+0
٥:	.0837733+0	1.9158960+00	6.	Ç (.2918856+0	.3231641+0
	0+2001991	CC+P1/5CD3-2	-1862844	S	.82014164	C+11+86+4.
0 0	1+9974567	2.54090904000	-6668664	ه د	. 3068100+0	3+04881011.
20	34846646	00.406.47711.7	-1140684	ې د	C+0060666.	> 0
07	.436833340	00+66/26+2-2	4989600-	ب	. > 320e46+0	•
;						
12	. 53480 f1+0	.3219389	2129722-0	9	.1394422+9	9
22	·6335940+C	3961015	. 5258158-3	2129060+0	. 7669889+0	9
53	.7350810+0	.4537253	.5375942-0	Ų (.4126533+3	2+0
54	.83926J7+C	.5127527	.5484168-0	ů.	.9755510+0	3+0
\$ 3	.9463904+0	.5671639	.5583754-0	Ò.	.7549951+9	9 + 0
9 ;	0+6584660*	6400/19.	0-6446196.	2 6	.4565054.	3+0
7 0 0	J-1995/91.	\$966T99•	6936430-0	2 5	0.007.7401.	2 4 4
2 0	398521146	7381100	5906083=0	58861354C	0+9641649	2
200	2.5175799+01	2.7696705+00	970842	\ ~	1.3964291+00	7.6370273+00
31	.63886640	1970057	6030186-	•	.1698309+0	.6974472+0
32	.7622181+0	.8196726	60828C5-	•	.6247C33-C	.7522240+0
33	764	2-8384740+00	307	7.3630182+00	7.6926053-01	7.8530229+00
*	.014946410.	.8537166	6174238-	•	.9015381-0	.8499146+0
35	.1439634+6	.8651689	6211983-	9	3032438-0	.8912677+0
9 9	-2746722+0	.8731220	6244384-	•	9956927-0	.9272550+6
25	-4067759+C	.6784281	6272034-	•	3-36362/9	3+1905856-
2 6	-5400/33+C	.8812342	6293503-	•	0-2681870	0+6799786
£ .	-6742769+0	.8820118	-6306360-	2 9	0-1868676.	3+64646
P	. 828 /90 /+0	.8821015	308672-	•	03+0000000	.9998848

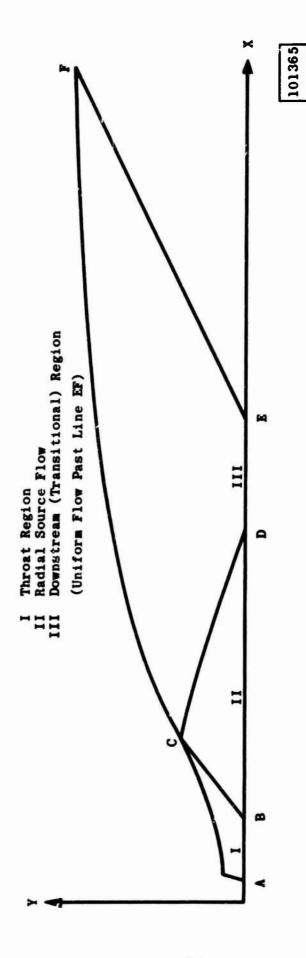


Fig. 7 Nozzle Configuration (Not to Scale)

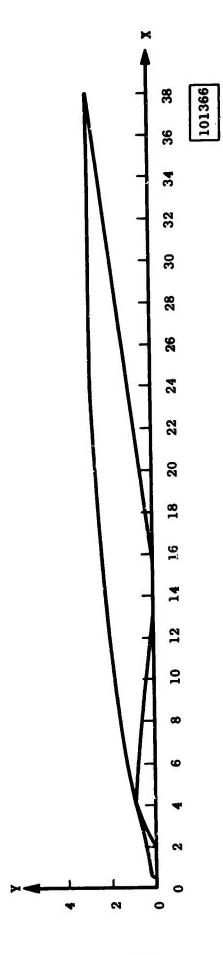


Fig. 8 Nozzle Configuration (to Scale)

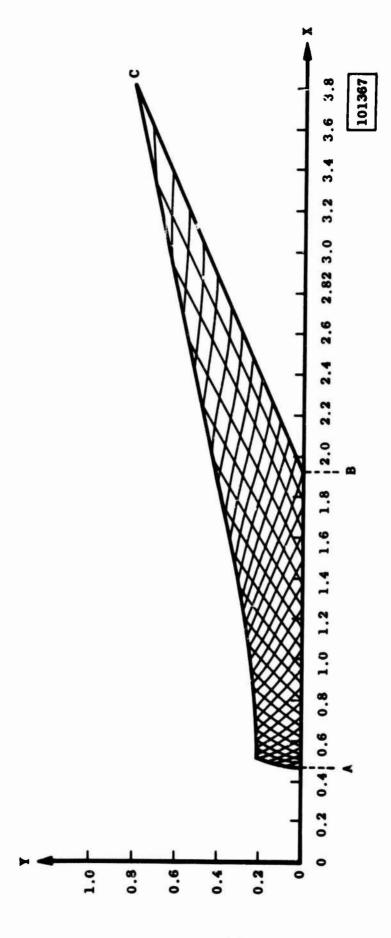


Fig. 9 Throat Region Showing Characteristic Network